Fluctuation-theorem method of measuring a particle's mass without knowing its shape or density

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ABSTRACT

Tracking the Brownian motion of aerosol particles as they settle in air allows a mass measurement. The particle typically falls downward at its terminal settling velocity; however, the particle occasionally will be displaced upwards due to Brownian fluctuations. The number of occurrences of upward and downward fluctuations is compared, using the formula for the work fluctuation theorem, to yield the mass. This method can be applied to either a single particle or a collection of particles. The advantages of this method include no required information about the size, shape, or density of the particle. Details of the analysis method are presented and illustrated with experimental data.

1. Introduction

The combined effects of fluctuating Brownian motion and steady terminal-velocity motion allow a measurement of particle mass, presented in this paper. In the force field of gravity alone, for a sufficiently small particle, the settling velocity diminishes enough that Brownian fluctuations can become prominent. Occasionally, the Brownian movements will briefly overcome the settling velocity, so that a particle's velocity can completely change sign. A free-falling particle can briefly be displaced "upwards" against the downward field of gravity. This motion against the force causing the drift can be interpreted as negative work done by the field on the particle, or an extraction of energy by the particle from the field. Such negative work extraction by the particle happens with a definite probability, predicted by the work fluctuation theorem (van Zon & Cohen, 2003). This theorem forms the basis of the mass measurement technique we report here.

In a previous communication (Wong, Goree, & Gopalakrishnan, 2018), we experimentally demonstrated the technique, using simple equipment including a settling chamber and a high-resolution video camera. By observing the trajectories of individual particles, histograms were constructed for the vertical displacements as particles fell under gravity. These histograms were then used to directly measure a mass for the falling particle, using the formula of the work fluctuation theorem. Advantages of this method, as described in Ref. Wong et al. (2018), include a simple apparatus, and an analysis method that requires no information about the particle's shape, density, or electric charge.

In this article, we present further details of the mass measurement method, with an emphasis on the practical implementation. We define the requirements that the apparatus must meet. We then list the analysis steps, which we illustrate in a step-by-step example using experimental data from our previous communication (Wong et al., 2018), using standard particles. We also discuss the factors that limit the mass range that can be accurately measured using this technique, and how they can be overcome with an enhanced...
design for the instrument.

2. Previous mass measurement methods

Mass plays such a prominent role in aerosol transport that many methods have been devised to obtain its value. We review many of these previous methods here.

One common approach to measure the mass of individual particles or the mass distribution of an aerosol population is integral detectors coupled to a classification mechanism. The classification mechanism separates particles based on a specific interaction with gas and/or external fields. These methods mainly are used to observe the aggregate effects of an aerosol particle population (Kulkarni et al., 2011). For instance, various online measurement techniques such as light scattering (Mulholland et al., 2013), differential mobility analysis (Hagen & Alofs, 1983; Knutson & Whitby, 1975a, 1975b; Wang & Flagan, 1990), diffusion battery methods (Sinclair, 1972; Sinclair, Countess, Liu, & Pui, 1976) and offline techniques such as electron microscopy are used to measure aerosol particle size distribution \( n(d_p) \). From the size distribution \( n(d_p) \), the mass distribution \( n(m_p) \) or its moments (average \( \bar{m} \) and variance \( \text{var}(m) \)) are inferred, rather than precise measurements of the mass of individual particles. The inference of the mass distribution of an aerosol from a measured size distribution \( n(d_p) \), although quite common, requires assumptions pertaining to the density (composition) and the morphology of measured particles. The measured “size” corresponds to either an interaction size such as the aerodynamic diameter, diffusion diameter, mobility diameter, sedimentation diameter or a geometric size inferred from electron microscopy. The mass distribution of the aerosol \( n(m_p) = \rho d_p^3 n(d_p) \) can be obtained in a straightforward manner if the shape and density of the particles are known or suitably assumed. These limitations of detectors based on classification mechanisms can be avoided using the new method described in this article.

Aerosol particles are not always spherical, so that it is desirable to have a mass measurement method that is independent of shape, like our method. While aerosols generated under homogenous residence times in a growth environment (exposure to concentration of condensing vapor and temperature history) develop into a nearly spherical shape and uniform composition (Feng et al., 1994), non-spherical particles with variable chemical composition and density are more common in atmospheric as well synthetic environments.

Previous methods with capabilities close to ours, for the measurement of the mass distribution of aerosols without assumptions about their shape or density, are the aerosol particle mass analyzer developed by Ehara and co-workers (Ehara, Hagwood, & Coakley, 1996) and the centrifugal particle mass analyzer developed by Olffert and co-workers (Olffert & Collings, 2005). These instruments introduce charged aerosol particles in the electric field that exists in the annular space between two cylinders rotating with respect to each other. The electric force and the centrifugal force on the particle are balanced by adjusting the rotation speed and applied voltage to infer the mass to charge ratio of the particles. By introducing particles of known charge state, the aerosol particle mass analyzer measures the mass distribution of an aerosol population without reference to a shape or density (Liao, Tseng, & Tsai, 2017; Lin et al., 2014; Tajima, Sakurai, Fukushima, & Ehara, 2013). When combined with electrical mobility analysis (Buckley, Kimoto, Lee, Fukushima, & Hogan, 2017; Chen, Ghosh, Buckley, Sankaran, & Hogan, 2018; Geller, Biswas, & Sioutas, 2006; Lall, Ma, Guha, Mulholland, & Zachariah, 2009; Lee, Widyastuti, Tajima, Iskandar, & Okuyama, 2009; Malloy et al., 2009), the aerosol and centrifugal particle mass analyzers have also been used to measure the two-dimensional size and mass distributions of different types of aerosols. The aerosol particle mass analyzer requires information about the charge state or charge distribution of the aerosol being measured. The charge of ambient and laboratory aerosols are often conditioned by exposing the particles to bipolar ions of approximately equal concentration in aerosol chargers. This allows the particles to attain a steady-state charge, size-dependent charge distribution. For particles <0.5 \( \mu \)m the charge distribution can be calculated using bipolar charging models (Gopalakrishnan, Meredith, Larriba-Andaluz, & Hogan, 2013; Wiedensohler, 1988). For particles \( \geq 0.5 \mu \)m the charge distribution is commonly assumed to have a Boltzmann profile (Gunn, 1954, 1955). Typically, a differential mobility analyzer is used upstream of the aerosol particle mass analyzer to introduce particles of known mobility (charge state and size), thereby making the inference of mass distribution possible (Scheckman, MCMurry, & Pratsinis, 2009). For aerosols of unknown charge distributions, the instrument yields the mass to charge ratio (Ehara et al., 1996).

3. Analysis method

3.1. Analysis steps to obtain the mass \( m_i \) of a single particle

Our fluctuation-theorem mass measurement requires, most importantly, a time series of vertical positions \( y(t) \) of particle \( i \). In addition, it requires the air temperature \( T \) and the gravitational constant \( g \). (The apparatus and measurement method for obtaining such a time series is discussed later, in Section 4.) From these inputs, the mass \( m_i \) of particle \( i \) can be obtained by choosing a value of \( \tau \) and following these seven steps.

1. First, divide the time series data \( y(t) \) of particle \( i \) into non-overlapping time segments of duration \( \tau \).
2. Second, compute the vertical displacement \( \Delta y_{t+\tau} = y(t+\tau) - y(t) \) of particle \( i \). This is repeated for each time segment.
3. Third, prepare a histogram by binning the computed values of the vertical displacement \( \Delta y_{t+\tau} \). The bins of the histogram are equally spaced and non-overlapping. We will use the symbol \( C \) to represent the value of \( \Delta y_{t+\tau} \) at the center of the bin. One can choose any positive value of \( C \); it will correspond to another bin at \(-C\). A histogram bin’s count, \( p(\Delta y_{t+\tau} = C) \), is the number of observations of \( \Delta y_{t+\tau} \) that fall within the bin centered at \( \Delta y_{t+\tau} = C \).
4. Fourth, using data from the histogram, compute
\[
\ln R = \ln \left[ \frac{p(\Delta y_{i,t} = C)}{p(\Delta y_{i,t} = -C)} \right],
\]

which we will term the displacement-count ratio. Each pair of counts in the histogram for bins centered at \(C\) and \(-C\) yields one value of \(\ln R\). The displacement-count ratio is computed not for just one value of \(C\), but for a wide range of values of \(C\).

(5) Fifth, plot the obtained values of the displacement-count ratio \(\ln R\) as the vertical axis of a graph, with the bin value \(C\) as the horizontal axis.

(6) Sixth, fit the plotted displacement-count ratio \(\ln R\) to a straight line to obtain the slope \(s\), for individual particle \(i\).

(7) Seventh, compute the mass \(m_i\) of the individual particle as

\[
m_i = -\left(\frac{k_B T}{g}\right)s_i,
\]

which also requires the air temperature \(T\), the Boltzmann constant \(k_B = 1.38 \times 10^{-23} \text{J/K}\), and the gravitational constant \(g\). Precise values of \(g\) for geographic locations are tabulated in standard references (Pavlis, Holmes, Kenyon, \& Factor, 2008).

Optionally, the step-by-step procedure above can be repeated with different choices of the parameter \(\tau\). For each value of \(\tau\), one will obtain one measurement of \(m_i\). All of these measurements can be averaged, if desired, to improve statistics.

This method can also be used to obtain the mass distribution \(n(m_i)\) of a population of particles. Obtaining \(n(m_i)\) requires time series of vertical positions for \(N\) particles belonging to the particle population. Then, simply repeating this procedure for each of the \(N\) time series will yield a sample of the mass distribution of the particle population. Practically speaking, if the particles are relatively monodisperse, a sample size of approximately \(N = 100\) should be sufficient to yield accurate estimates of \(n(m_i)\).

Detailed derivations of the equations used in this section are provided in Appendix B.

3.2. Extension of method to obtain the average mass \(m_{\text{avg}}\) of many particles

Instead of the mass of a single particle \(m_i\), one can instead obtain the average mass \(m_{\text{avg}}\) of \(N\) particles, if all the particles have a similar mass. The input data required are time series of vertical positions \(y(t)\) for each of the \(N\) particles. The steps for obtaining \(m_{\text{avg}}\) are nearly identical to the steps provided in Section 3.1 above, but with a few minor changes as listed below.

Steps (1) and (2) are repeated for each of the \(N\) particles and their position time series \(y(t)\).

In step (3), the histogram is built for data combined for all \(N\) particles.

Step (6) will yield a slope \(s_{\text{avg}}\), based on a single graph of data.

For step (7), Eq. (2) is

\[
m_{\text{avg}} = -\left(\frac{k_B T}{g}\right)s_{\text{avg}}.
\]

When obtaining the average mass \(m_{\text{avg}}\) of many particles it is typically optimal to combine the histogram data of vertical displacements \(\Delta y_i\) before computing the displacement-count ratio \(\ln R\) and finding its slope \(s_{\text{avg}}\), as opposed to computing \(\ln R\) and \(s\) for each particle and averaging the slopes to obtain \(s_{\text{avg}}\). This suggested sequence of steps helps minimize the finite-size effects in the histogram counts, since upward displacements can be rare when a single particle is tracked for a short time.

3.3. Example of analysis method

Here we present a step-by-step analysis of experimental data, using the steps provided in Sections 3.1 and 3.2. The data are from our demonstration experiment, which we reported in Ref. Wong et al. (2018). We start with position time series data for \(N = 69\) particles. Sample time series of particle positions are shown in Fig. 1. The vertical motion of the particles, in Fig. 1(a), is mostly a downward trend that corresponds to a terminal settling velocity. On occasion, the particles are displaced upward against the force of gravity due to Brownian motion, as shown in the inset. Observations of these upward fluctuations are crucial for our mass measurement method. Details of the demonstration-experiment apparatus are provided in the Section 4.2.

We began by choosing a time duration \(\tau = 25\) ms. For step (1), the position time series \(y(t)\) of each particle \(i\) was divided into 25 ms intervals. Next, for step (2) we compute the vertical displacement \(\Delta y_{i,t} = y(t + \tau) - y(t)\) for each of the time segments, which yields 40, 870 observations of \(\Delta y_{i,t}\). For step (3), we bin and count the observations of \(\Delta y_{i,t}\) to produce the histogram presented in Fig. 2(a).

For step (4), we choose a pair of bins from the histogram that are centered at the value \(\Delta y_{i,t} = C\) and the corresponding value \(\Delta y_{i,t} = -C\). The counts within these bins are used as the input for Eq. (1) to compute a single value of the displacement-count ratio \(\ln R\). We repeat this process for all pairs of bins in the histogram; one example pair of histogram bins, and the corresponding computed value of \(\ln R\), is indicated by arrows in Fig. 2.

For step (5), we prepare a graph with the obtained values of the displacement-count ratio \(\ln R\) as the vertical axis, and the histogram bin value \(C\) as the horizontal axis. This graph is presented in Fig. 2(b). We next, for step (6), fit a straight line through the plotted values of \(\ln R\), yielding the slope \(s_{\text{avg}} = -1.94 \mu\text{m}^{-1}\).

For step (7), we use Eq. (3) to obtain the average mass \(m_{\text{avg}} = 8.073 \times 10^{-16}\) kg for the \(N = 69\) particles. The inputs for the
For this demonstration, we choose to perform the optional averaging, repeating steps (1)-(7) for multiple values of the specified time duration $\tau$. We choose six values of $\tau$ in the range of 30 ms to 55 ms. Each value of $\tau$ yields a separate mass measurement, which we average to decrease the size of error bars, yielding our final mass measurement $m_{\text{avg}} = (8.07 \pm 0.10) \times 10^{-16}$ kg for the 69 particles that we analyzed.

For comparison, we obtained a reference mass measurement of $m_{\text{avg}} = (8.13 \pm 0.11) \times 10^{-16}$ kg for the $N = 69$ particles, which agrees within error bars with our fluctuation-theorem-method measurement. This reference measurement had the limitation that it requires particles to be spherical (unlike the fluctuation-theorem method, which places no constraints on particle shape). The inputs for the reference mass measurement were the particles’ terminal settling velocity and average horizontal diffusion coefficient, as well as the air temperature $T$ and gravitational constant $g$.

4. Apparatus

4.1. Requirements

A simple implementation of the mass measurement method is possible, with only two main requirements. The force requirement is that the particle must undergo free-fall with no disturbing forces other than gravity. In the simplest case, the particle will fall in still air to avoid wind-like forces. The tracking requirement is that the particle’s vertical motion must be observed to yield a position time.
series $y(t)$. This tracking can be done with a video camera and image-analysis software. Additionally, the air temperature $T$ and the gravitational constant $g$ are required.

### 4.2. Design for demonstration experiment

A two-chamber apparatus, shown in Fig. 3, was used in our demonstration experiment. Particles were dropped from the disperser in the upper chamber, and fell through a 6-mm diameter opening into the lower chamber. This apparatus has a simple design, without any powered electrodes, instruments for electric charging of particles, or power supplies to exert forces on the particle.

To meet the force requirement, the two-chamber design minimized convection currents in the lower chamber. To accomplish this, the lower chamber had a small height so that any temperature gradient is unlikely to cause the critical Rayleigh number to be exceeded. Furthermore, the top and bottom walls of the chambers were grounded to eliminate disturbing electric fields.

To meet the tracking requirement, particles were illuminated by a sheet of laser light and imaged by a side-view video camera within the lower chamber. The camera was a Phantom Miro M120 that imaged at 200 frames/s. The image-analysis software that was used was ImageJ (Feng, Goree, & Liu, 2007) This setup for illumination and imaging was adequate to track micron-sized particles.

The particles that we used in the demonstration experiment were polymer (melamine formaldehyde) and were nominally $1.04 \mu m$

![Fig. 3. Sketch of the demonstration-experiment apparatus, as viewed from the (a) top and (b) side. The force requirement was met by the glass walls and grounded metal plates that eliminated air currents and stray electric fields. The tracking requirement was met by imaging particles with a video camera. A 15-mW HeNe laser beam was shaped to illuminate falling particles within a vertical cross section of the lower chamber. The optics used for the illumination, not drawn to scale, include: mirrors M1 and M2, spherical lenses L1 and L2, and cylindrical lens L3. A thermometer, not shown here, recorded the room temperature. This figure is a reproduction of Figs. 1(a) and (b) from Wong et al. (2018).](image1)

![Fig. 4. Particles from the same bottle as used in our demonstration experiment imaged with a transmission electron microscope. The spherical shape of the particles is not necessary for the fluctuation-theorem mass measurement method. This figure is a reproduction of Supplemental Fig. 1 from Ref. Wong et al. (2018).](image2)
in diameter according to the manufacturer’s specifications. Particles were confirmed to be spherical, Fig. 4.

4.3. Approach for incorporating the method in a continuous flow system

Continuous flow systems with multiple devices are often used to sample, measure, and transport aerosols. It may be attractive to couple the fluctuation-theorem mass measurement method with other measurement systems, such as differential mobility analyzers or diffusion batteries.

We suggest one possible implementation here. A gas containing the particles can be flowed through a measurement volume, where individual particles are tracked using video cameras to yield time series of their vertical positions, as in our demonstration experiment. The gas flow is required to be steady and laminar, so that its effect on a particle motion can be completely characterized and, if necessary, removed. For example, if the flow has a vertical component, then the constant displacement that a particle experiences due to the flow must be subtracted from the particle’s vertical positions. On the other hand, if the gas flow is entirely horizontal (perpendicular to the gravitational force), then no changes to the analysis steps would be required.

4.4. Design for an extended mass measurement range

Our mass measurement method worked well with data from our demonstration experiment for 1-micron particles. Smaller particles could in principle be measured using exactly the same method. The only challenge for smaller particles is obtaining sufficient light scattering, for tracking.

For larger particles, we can propose an enhancement to the apparatus. The problem that must be avoided, with large particles, is that they will fall too fast with too few upward displacements. This problem can be remedied by changing either the accelerating field or the damping force. In our demonstration experiment, the accelerating field was simply a 1-g gravitational acceleration, and the damping force was gas drag at atmospheric pressure.

We can reduce the accelerating field by adding an electric force that opposes gravity. This approach requires applying a known charge \( q \) to each particle, and it also requires electrodes to apply a uniform electric field throughout the measurement volume. In this approach, Eq. (2) becomes

\[
m_i = -\left( \frac{k_B T}{g} \right) s - \frac{q E}{g}.
\]

By increasing the air pressure, one can reduce the settling velocity. In this way, the observation time is increased so that the number of observations of upward displacement is adequate. The analysis procedure and formulas would be the same as in Section 3.1.

5. Choosing \( \tau \)

Minimizing the uncertainty of the mass measurement relies on improving the counting statistics for the histogram of \( \Delta y_{i,\tau} \). In particular, the histogram should have a large number of counts for upward displacements. Parameters in the experiment and analysis can be chosen to provide the best conditions for observing a sufficient number of these upward displacements. Here, we discuss the choice of the specified time interval \( \tau \).

An appropriate value for \( \tau \) can be determined by examining the experimental data. The main requirement is that the histogram should include a significant number of upward displacement events. As a starting point, one can vary \( \tau \) until the histogram’s mean value and half-width are comparable, which typically occurs when \( \Delta y_{i,\text{term}} \approx kT \). Here \( y_{i,\text{term}} \) is the terminal settling velocity of particle \( i \).

Since one obtains a measurement of mass for each value of \( \tau \), it can be desirable to repeat the measurement analysis for several values of \( \tau \), as discussed above in Section 3.1. The measured masses can be averaged to help improve statistics, and the variations in the measured masses can help quantify the measurement uncertainty.

Besides the factors mentioned above, which center on statistics, in an extreme case one could encounter a physical limitation in the method by choosing too short a value of \( \tau \). This physical limitation concerns the asymptotic-limit requirement of the fluctuation theorem (Wong, Goree, Haralson, & Liu, 2017). A possible symptom of this problem would be a detectable trend in the data for mass measurement vs \( \tau \).

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Appendix A. Impact of air temperature and pressure on mass measurement

The air within the apparatus acts as a thermal bath for particles that are falling through it. The air temperature \( T \) affects the size of
fluctuations in particle motion; a higher $T$ leads to larger random particle displacements, and likewise, a lower $T$ leads to smaller random particle displacements. In particular, a higher $T$ may be helpful when measuring the mass of larger particles that may otherwise have fluctuations too small to resolve.

Errors associated with air temperature $T$ are most likely associated to either a systematic error in the measured $T$ or air currents driven by temperature gradients. First, a systematic error in the measured $T$ leads to a proportionally sized error in the measured mass, as can be seen by inspecting Eq. (2). For example, a 1% systematic error in temperature (approximately 3 K at room temperature) would lead to a 1% error in the measured mass. Second, air currents driven by temperature gradients can do work on an otherwise free-falling particle, so that the method may no longer be applicable. Precautions in the apparatus design should be taken to minimize temperature gradients or their effects (such as the chamber height consideration discussed in Section 4.2).

The air pressure within the apparatus affects not only the size of fluctuations in particle motion, but also the terminal settling velocity. Higher air pressures lead to smaller fluctuations and slower settling velocities, while lower air pressures lead to larger fluctuations and faster settling velocities. Conveniently, these air-pressure effects cancel out when using the fluctuation-theorem method, so that the resulting mass measurement is independent of air pressure (i.e. air pressure does not enter any equation used in the method). Since the fluctuation-theorem method is valid at any pressure, the air pressure should be chosen to optimize particle motion to allow for precise tracking. In particular, the video cameras must be able to resolve the size and duration of upward displacements of particles.

Appendix B. Derivations

Here we provide derivations of Eqs. (1) and (2).

For a particle $i$ undergoing free fall due to gravity, the work $W_{i,t}$ done during a time interval $\tau$ is given by

$$W_{i,t} = -m_i g \Delta y_{i,t}.$$  \tag{B.1}

This quantity can be normalized by $k_B T$ to yield the normalized work,

$$w_{i,t} = -\frac{m_i g \Delta y_{i,t}}{k_B T}.$$ \tag{B.2}

The work fluctuation theorem of van Zon and Cohen (2003) predicts that the normalized work $w$ will obey

$$\ln \frac{p(w_{i,t} = C')}{p(w_{i,t} = C^*)} = -C', \text{ as } \tau \to \infty.$$ \tag{B.3}

To implement this formula using experimental data, $p(w_{i,t} = C')$ is the number of counts in a histogram of observations of $w_{i,t}$. In particular, $p$ is the number of counts within a histogram bin centered at $C'$. Substituting Eq. (B.2) into the left-hand side of Eq. (B.3) yields

$$\ln \left[ \frac{p\left(\frac{-m_i g \Delta y_{i,t}}{k_B T} = C'\right)}{p\left(\frac{-m_i g \Delta y_{i,t}}{k_B T} = C^*\right)} \right] = -C', \text{ as } \tau \to \infty.$$ \tag{B.4}

The limit $\tau \to \infty$ requires, in practice, a value of $\tau$ large enough to achieve a convergence of the two sides of this equation. Such a convergence time requires an adequate number of stochastic fluctuations, for example due to Brownian motion. Substituting a chosen value

$$C' = C' \frac{m_i g}{k_B T}$$ \tag{B.5}

in Eq. (B.4) gives

$$\ln \left[ \frac{p(\Delta y_{i,t} = C)}{p(\Delta y_{i,t} = -C)} \right] = \frac{m_i g C}{k_B T}, \text{ as } \tau \to \infty,$$ \tag{B.6}

which we can write as $\text{LHS} = \text{RHS}$.

Finally, we see that the mass $m_i$ can be obtained from the derivative $(\text{LHS})/dC$. This result leads us to the prescription of steps (6) and (7) of our procedure. The mass $m_i$ is found from the slope $s_i$ of a graph of the LHS vs $C$.

References


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